

COMPOSITE SHEET MATERIALFIELD OF THE INVENTION

This invention relates to a moisture vapor permeable, substantially liquid impermeable composite sheet structure useful in medical garments.

5 More particularly, the invention is directed to a composite laminated sheet comprising a thin extruded moisture vapor permeable film sandwiched between two nonwoven webs, at least one of which is a powder-bonded nonwoven web. The composite laminated sheet acts as a barrier to liquids, bacteria, viruses and odors, and yet is also highly permeable to moisture

10 vapor.

BACKGROUND OF THE INVENTION

The use of laminates of films and nonwovens for medical applications, including medical garments, is known in the art. For example, Shehata, U.S. Patent 5,445,874 describes laminates that are waterproof, blood-proof, and virus proof with a high moisture vapor transmission rate.

15 The laminates include a solid extruded film layer of a polymer comprising 60-70% butylene terephthalate units and the balance a polyester glycol sandwiched between two woven or nonwoven fabrics. The thickness of the film layer is typically between about 0.75 to about 3 mil (19 to 76 micrometers) and can be extruded directly onto one of the fabric layers.

20 Alternately, the film layer can be extruded onto a release layer or can be extruded as a blown film. The films can be laminated onto the fabric by powder lamination, hot melt lamination, and wet adhesive lamination. The laminates are suitable for use in re-usable clothing or apparel where it is desirable or necessary to prevent liquids from penetrating through to the wearer's skin. Garments made from the laminates are washable and sterilizable a minimum of 100 times.

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PCT Publication No. WO 97/45259 to Carroll et al. discloses a breathable composite sheet material comprised of a moisture vapor permeable thermoplastic film adhered to a fibrous substrate. The breathable thermoplastic film is primarily comprised of a thermoplastic polymeric material selected from the group of block copolyether esters, block copolyether amides and

polyurethanes. The fibrous substrate is a nonwoven sheet made primarily of polymeric fibers that are incompatible with the film, such as a polyolefin fibers. The film is adhered to the fibrous substrate by extruding a layer of the molten film-forming polymer directly onto the fibrous substrate and then mechanically 5 engaging the film and the fibers of the substrate, as for example by pressing the molten film into the fibrous substrate in a nip formed between two rolls.

Adhesive lamination, thermal lamination and extrusion coating methods have all been used to produce composite sheets of a fibrous nonwoven substrate and a moisture vapor permeable, substantially liquid 10 impermeable film. It has been possible to make such composite sheets with good barrier properties so long as the moisture vapor permeable film is relatively thick (*i.e.*, greater than about 25 micrometers). However, it has been difficult to make such composite sheets with thinner films without sacrificing important barrier properties. Very thin moisture vapor permeable 15 films are desirable in a composite sheet because thinner films facilitate greater flux of moisture vapor through the composite sheet and because thinner films use less of the film material and are accordingly less expensive to produce.

Adhesive lamination is carried out in a post film formation step. 20 For adhesive lamination to be feasible, the moisture vapor permeable film must have enough tensile strength and tear strength so that the film can be formed, wound onto a roll, and later unwound and handled during the adhesive lamination process. It is difficult to handle moisture vapor permeable films less than about 1 mil (25 micrometers) in thickness during 25 the adhesive lamination process without tearing the film or introducing defects into the film.

Thermal lamination of moisture vapor permeable films less than 25 micrometers thick has resulted in composite sheet materials with inadequate barrier properties. When composite sheets are made by 30 thermally laminating a thin film to a fibrous substrate, the thin film handling problems associated with adhesive lamination, as described above, are encountered. In addition, to carry out a thermal lamination, the film must be

subjected to elevated temperatures and pressures so as to soften the film and force it into mechanical engagement with the fibrous substrate. Generally, the bond strength between the film and the fibrous substrate increases with increasing lamination temperatures and increasing nip pressures.

- 5 Unfortunately, when moisture vapor permeable films with a thickness of less than 25 micrometers are subjected to the increased temperatures and pressures needed to obtain adequate bond strength between the layers in the composite sheet, small holes can develop in the film such that the composite sheet does not exhibit the barrier properties desired in a composite sheet for
10 use in medical apparel.

- It is the practice in many hospitals to use surgical gowns only once, and to discard the gowns thereafter. There remains a need for breathable sheet materials having a high barrier level to viral penetration and which also can be prepared at low cost for use in single-use disposable
15 medical garments. An ideal material must also be strong enough so that it does not rip or delaminate under normal use regardless of whether the material is dry or wet. Where the sheet material is to be used in apparel, it is also important that the material be flexible, soft and drapable. In addition, where the sheet material is to be used in medical apparel, it is important that
20 the sheet not generate fiber lint that might contaminate a medical environment.

SUMMARY OF THE INVENTION

- One embodiment of the present invention is a moisture vapor
25 permeable, substantially liquid impermeable composite sheet material comprising a moisture vapor permeable monolithic polymeric film having a first side and a second side, a first nonwoven layer comprising a moisture vapor permeable powder-bonded nonwoven layer, said powder-bonded layer comprising a nonwoven web of fibers, wherein greater than 95 weight percent
30 of the fibers in the nonwoven web are compatible with said polymeric film, said first nonwoven layer being adhered to the first side of the polymeric film by extrusion of said film onto said first nonwoven layer, and optionally a

second moisture vapor permeable nonwoven layer adhered to the second side of the film.

Another embodiment of the present invention is directed to a garment or other protective cover prepared from a moisture vapor permeable, 5 substantially liquid impermeable composite sheet material comprising a moisture vapor permeable monolithic polymeric film having a first side and a second side, a first nonwoven layer comprising a moisture vapor permeable powder-bonded nonwoven layer, said powder-bonded layer comprising a nonwoven web of fibers, wherein greater than 95 weight percent of the fibers 10 in the nonwoven web are compatible with said polymeric film, said first nonwoven layer being adhered to the first side of the polymeric film by extrusion of said film onto said first nonwoven layer, and optionally a second moisture vapor permeable nonwoven layer adhered to the second side of the film.

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BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings, which are incorporated in and constitute a part of this specification, illustrate the presently preferred embodiments of the invention and, together with the description, serve to 20 explain the principles of the invention.

Figure 1 is a cross-sectional view of the composite sheet structure of the invention.

Figure 2 is a schematic representation of a process by which the powder-bonded nonwoven layer of the composite sheet of the invention is 25 extrusion coated with the film layer.

Figure 3 is a schematic representation of an alternate process in which a bilayer film is co-extruded onto the powder-bonded nonwoven layer.

DETAILED DESCRIPTION

30 The term "compatibility" as used herein, refers to the degree to which polymer materials are miscible with each other and/or interact with each other. "Incompatible" materials, as used herein, means materials that are substantially immiscible with each other or do not interact with each other.

Incompatible materials do not wet or adhere well to each other, even when heated. As used herein, "compatible" materials are materials that are not "incompatible" with each other, as defined above. For purposes of this application, a fiber is deemed to be compatible with a synthetic adhesive or

- 5 with another polymer if the adhesive or other polymer is miscible with material that comprises the majority of the fiber and if the adhesive or other polymer readily wets the fiber or if the adhesive or polymer can adhere well to the fiber.

The term "nonwoven fabric, sheet, layer, or web" as used herein
10 means a structure of individual fibers or filaments that are positioned in a random manner to form a planar material without an identifiable pattern by means other than knitting or weaving. As used herein, the term "fiber" means an elongated strand of defined length, such as staple fibers formed by cutting a continuous strand into lengths and the term "filament" means a generally
15 continuous strand that has a very large ratio of length to diameter.

The terms "powder-bonded nonwoven web and powder-bonded nonwoven layer" as used herein refer to a bonded nonwoven fabric formed by depositing a powder adhesive onto an unbonded fibrous web, such as a carded web, in a way that the powder adhesive is distributed throughout the
20 thickness of the fibrous web. A powder adhesive is selected which melts at a temperature below the melting point of the fibers in the fibrous web. Thereafter, the powder-containing web is heated to melt the powder adhesive without melting the fibers of the fibrous web to form a powder-bonded nonwoven web. Powder-bonded nonwoven fabrics are distinguished from
25 sheets made using powder lamination methods such as those described in Shehata U.S. Patent No. 5,445,874 where an activated web consisting of an adhesive material is formed from an adhesive powder. In powder lamination, the powder adhesive bonds two substrates together, such as a woven or nonwoven substrate with a film layer and the adhesive powder is
30 concentrated primarily at the interface between the two substrates. In powder lamination, the powder adhesive does not contribute to any significant degree to the bonding within the nonwoven substrate.

The term "spunbond" as used herein means a nonwoven sheet formed by melt extrusion of a polymer into strands that are quenched and drawn, usually by high velocity air, to strengthen the filaments. The filaments are collected on a forming surface and bonded, often by application of heat and pressure using a patterned bonding roll.

As used herein, the "machine direction" is the long direction within the plane of a sheet, i.e., the direction in which the sheet is produced. The "cross direction" is the direction within the plane of the sheet that is perpendicular to the machine direction.

As used herein, the term "laminate" means a composite material made from two or more layers or webs of material which have been bonded or otherwise attached to one another.

Referring to Figure 1, the composite laminated sheet 10 of the current invention is shown. Composite laminated sheet 10 comprises a moisture vapor permeable powder-bonded nonwoven layer 12 onto which a substantially liquid impermeable, moisture vapor permeable polymer film 14 is extrusion coated. Film 14 can be a single layer or multi-layer film. An optional second moisture vapor permeable nonwoven layer 16 can be adhered to the film layer on the side of the film layer opposite that which is adhered to the powder-bonded nonwoven layer.

The powder-bonded nonwoven layer 12 used in the composite laminated sheet of the invention is prepared using methods known in the art, such as the process described in Zimmerman et al. U.S. Patent 4,845,583. A carded web of staple fibers is optionally passed through a web spreading section prior to applying a powdered adhesive material. Preferably the staple fibers of the carded web have a length between about 1 and 2 inches (2.54 to 5.08 cm) and a denier between 1 and 2 denier per filament (1.1 to 2.2 dtex). An adhesive powder is applied to the carded web using a powder-depositing device. The powder drops onto the web and is distributed through the web by gravity. Excess powder falls through the web and is collected for recycling. The weight of powder deposited in the carded web is preferably from about 8 to about 30 weight percent, and more preferably between about 15 to 25

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weight percent based on the total weight of the carded web and adhesive powder. Bonding of the nonwoven layer can be achieved by applying heat to the powder-infiltrated web. For example, the web can be passed through an oven, such as an infrared oven in which the adhesive powder fuses and bonds 5 the fibers of the web at fiber crossover points where the fibers and the bonding material come into contact. Upon leaving the oven, the web is subjected to light pressure by means of a nip roll. The powder-bonded nonwoven layer preferably has a basis weight in the range of 13.8 g/m² to 60 g/m², more preferably in the range of 16 g/m² to 34.5 g/m², and most preferably 16 g/m² to 10 29.6 g/m².

Powder-bonded nonwoven layer 12 is preferably prepared from a carded web of staple fibers, in which the fibers are comprised of a synthetic polymer that is compatible with both the polymer of film layer 14 and the adhesive powder used bond the staple fibers in the powder-bonded 15 nonwoven layer. Preferably at least 90 weight percent of the staple fibers in the carded web, based on the total weight of staple fibers in the carded web comprise fibers that are compatible with both the film layer and the adhesive powder. More preferably greater than 95 weight percent of the staple fibers in the carded web comprise fibers which are compatible with the adhesive 20 powder and the film layer. As the level of incompatible staple fibers in the carded web is raised above about 10 weight percent, the degree of bonding in the powder-bonded nonwoven layer is reduced which can result in a powder-bonded nonwoven layer with reduced strength which can cause handling problems as well as increased linting. In end uses such as medical 25 garments and drapes, linting is especially undesirable.

The fibrous components of the powder-bonded nonwoven layer preferably comprise a polyester such as poly(ethylene terephthalate), poly(1,3-propylene terephthalate) and copolymers thereof. Such polyester polymers are compatible with block polyether copolymers such as a block 30 polyether ester copolymers, with polyurethane copolymers, with poly(etherimide) ester copolymers, and with combinations thereof. One type of polyester fiber that can be used are shaped polyester fibers, such as

shaped polyester fibers with a scalloped-oval cross-section as disclosed in U.S. Patent 3,914,488 to Garrafa (assigned to DuPont). It is believed that where the polyester fibers comprise at least 10% of such shaped fibers, channels are created in the fibrous substrate through which moisture vapor

- 5 can be more efficiently conveyed through the composite laminated sheet. Alternately, a laminate of a powder-bonded polyamide nonwoven and a poly(etheramide) film can be used.

The powder adhesive that is used in the powder-bonded nonwoven layer is comprised of a thermoplastic polymer that melts at a 10 temperature below the melting point of the staple fibers used in the carded web. A powder adhesive is selected which is compatible with the film layer as well as with at least 90 weight percent, and preferably greater than 95 weight percent, of the staple fiber components of the carded web so as to provide good bonding both within the powder-bonded nonwoven layer as well as 15 between the powder-bonded nonwoven layer and the film layer which is extruded thereon.

In a preferred embodiment, the powder-bonded nonwoven layer is prepared from a carded web of polyester staple fibers and a polyester copolymer adhesive powder. Suitable polyester copolymer adhesive powders 20 include polyester copolymer powders such as those available from EMS-American Grilon, Inc. Typical copolyester adhesives have melting points of from 100 to 130 °C. and are available as coarse powders (200-420 micrometers or 70-40 U.S. standard mesh), medium powders (80-200 micrometers or 200-70 U.S. standard mesh) and fine powders (80 25 micrometers or less, or finer than 200 U.S. standard mesh), the medium powders being preferred when mechanical applicators are used to apply the adhesive powder to the web.

Film layer 14 comprises a polymeric material that can be extruded as a thin, continuous, moisture vapor permeable, and substantially liquid 30 impermeable film. The film layer is extruded directly onto the powder-bonded nonwoven layer and adheres to both the fibrous and adhesive components of the powder-bonded web. Preferably, the extruded film is less than about 1

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mil (25 micrometers) thick, more preferably less than about 0.75 mil (19 micrometers) thick, and most preferably less than about 0.60 mil (15.2 micrometers) thick. The film layer 14 is preferably comprised of a block polyether copolymer such as a block polyether ester copolymer, a 5 polyetheramide copolymer, a polyurethane copolymer, a poly(etherimide) ester copolymer, polyvinyl alcohols, or a combination thereof. Preferred copolyether ester block copolymers are segmented elastomers having soft polyether segments and hard polyester segments, as disclosed in Hagman, U.S. Patent No. 4,739,012. Suitable copolyether ester block copolymers are 10 sold by DuPont under the name Hytrel®. Hytrel® is a registered trademark of DuPont. Suitable copolyether amide polymers are copolyamides available under the name Pebax® from Atochem Inc. of Glen Rock, New Jersey, USA. Pebax® is a registered trademark of Elf Atochem, S.A. of Paris, France. Suitable polyurethanes are thermoplastic urethanes available under the name 15 Estane® from The B.F. Goodrich Company of Cleveland, Ohio, USA. Suitable copoly(etherimide) esters are described in Hoeschele et al., U.S. Patent 4,868,062.

A preferred film comprises a layer of nonporous (monolithic) copolyether ester copolymer. Monolithic copolyether ester membranes such 20 as those made of Hytrel® copolyether ester elastomer, sold by DuPont, absorb water from the "wet" side of the membrane into the polymer matrix and release the water from the "dry" side, a process which has been referred to in the art as pervaporation. The rate at which water vapor is released on the dry side of a Hytrel® film depends on the amount of water that has 25 diffused into the membrane, which in turn depends on the relative humidity on the wet side of the membrane. At very high relative humidity, or when liquid water is in contact with the membrane on the wet side, the water vapor transmission rate of a Hytrel® membrane can be extremely high.

The film layer 14 is preferably applied to the powder-bonded 30 nonwoven layer by extrusion coating. In an extrusion coating process, a uniform (monolithic) molten extrudate is coated onto the powder-bonded nonwoven layer. The molten polymer and the powder-bonded web are

brought into intimate contact as the molten polymer cools and bonds with the web. Such contact and bonding can be enhanced by passing the layers through a nip formed between two rolls. Alternatively, the molten polymer can be pulled into contact with the powder-bonded nonwoven web by passing the
5 coated web over a suction inlet such that a vacuum pulls the molten polymer into contact with the web as the polymer cools and bonds with the web.
During the extrusion coating process, some or all of the powder adhesive in
the powder-bonded nonwoven web may melt, which is believed to provide
improved bonding between the thin film layer and the powder-bonded
10 nonwoven web. The bonding between the polymeric film layer and the
adhesive present in the powder-bonded nonwoven web is believed to make it
easier to produce a very thin moisture vapor permeable film that is
substantially free of pinholes or other defects, yet which has a relatively high
rate of moisture vapor transmission. As used herein, "pinholes" means small
15 holes inadvertently formed in a film either during manufacture or processing
of the film.

One preferred means for applying the film layer to the powder-bonded nonwoven layer is illustrated in Figure 2. Melt-processable polymer is fed in pellet form, along with any additives, into an inlet 26 of an extruder
20 hopper 24, preferably under a nitrogen purge. The polymer is melted and mixed in a screw extruder 20 at a screw speed in the range of 100 to 200 rpm, depending on the dimensions of the extruder and the properties of the polymer. The melted mixture is discharged from the extruder under pressure through a heated line 28 to a flat film die 38. The polymer is discharged from
25 the flat film die 38 at a temperature above the melting temperature of the polymer, and preferably at a temperature in the range of 180 °C to 240 °C. The polymer melt 40 discharging from the flat film die 38 coats the powder-bonded nonwoven layer 12 which is provided from supply roll 30.

Preferably, the powder-bonded nonwoven web 12 passes under
30 the die at a speed that is coordinated with the speed of the extruder so as to obtain a very thin film that preferably has a thickness of less than 25 micrometers. The coated powder-bonded nonwoven web enters a nip formed

between nip roll 35 and roll 36, which rolls are maintained at a temperature selected to obtain a composite laminated sheet with a desired bond strength and moisture vapor permeability. The temperature of rolls 35 and 36 is preferably within the range of 10 °C to 120 °C. Higher roll temperatures yield 5 a composite sheet having higher bond strength, while lower roll temperatures yield composite sheets with higher moisture vapor permeability. Preferably, nip roll 35 is a smooth rubber roll with a low-stick surface coating while roll 36 is a metal roll. Nip roll 35 can also have a matte or textured finish to prevent sticking of the film layer. A textured embossing roll may be used in place of 10 the metal roll for the roll 36 if a composite laminated sheet with a more textured film layer is desired. Passing the coated web through the nip formed between cooler rolls 35 and 36 quenches the polymer melt while at the same time pressing the polymer melt 40 into contact with the fibers and adhesive of 15 the powder-bonded nonwoven layer 12. A water dip pan 56 with associated roll 58 can be used to increase the quench rate and to prevent sticking. The nip pressure applied should be sufficient to achieve the desired degree of bonding between the film and the nonwoven layer but not so great as to create pinholes in the film layer. The powder-bonded nonwoven/film laminate 20 10 is transferred from the roll 36 to another smaller roll 39 before being wound up on a collection roll 44. The coated composite laminated sheet 10 is transferred from the roll 36 to another smaller roll 39 before being wound up on a collection roll 44.

The second nonwoven layer 16 (Fig. 1) can optionally be fed into the nip on the side of the film layer opposite the side to which the powder- 25 bonded nonwoven layer 12 is adhered. When the second nonwoven layer is incorporated into the composite laminated sheet in this manner, the side of the second nonwoven layer contacting the film layer will generally be adhered to the film layer over substantially the entire surface thereof. This can result in a composite laminated sheet that is stiffer than desired for medical 30 garments or other apparel end uses due to the high degree of bonding between the film layer and both the powder-bonded nonwoven layer and the second nonwoven layer. If the second nonwoven layer is made of polymeric

fibers or filaments which are incompatible with the film layer, the bond strength between the film and the second nonwoven layer may be so low as to cause the second nonwoven to delaminate from the film layer during use. Preferably the bond strength between the film and the second nonwoven

5 layer is at least 50 grams/inch when the composite sheet material is either wet or dry, more preferably between 50 and 300 grams/inch.

The film layer 14 (Fig. 1) of the composite laminated sheet can be comprised of multiple layers. Such a film may be co-extruded with layers comprised of one or more of the above-described breathable thermoplastic

10 film materials. Examples of such multiple layer moisture vapor permeable films, which typically comprise a comparatively more hydrophobic elastomer layer and a comparatively more hydrophilic elastomer layer, are disclosed in Ostapchenko, U.S. Patent No. 4,725,481. In a preferred embodiment, a multi-layer film (in a bi-layer execution) is extruded onto the powder-bonded

15 nonwoven layer 12 with the comparatively more hydrophobic elastomer layer facing outwardly from the powder-bonded web and the comparatively more hydrophilic elastomer layer bonded to the powder-bonded nonwoven layer. Typically, for a given thickness, the hydrophobic elastomer layer exhibits a lower moisture vapor transmission rate than the hydrophilic elastomer layer

20 due to its comparatively lower moisture content under in-use conditions. However, when employed in a comparatively thin layer, the effect of the hydrophobic lower moisture content film layer does not significantly diminish the moisture vapor transmission rate of the overall composite laminated sheet. Preferably, the comparatively more hydrophobic elastomer comprises

25 between 20 and 30 percent of the total thickness of the composite film layer. Medical garments are preferably manufactured from the composite laminated sheet of the invention with the second nonwoven layer facing outwardly, away from the person wearing the garment. The comparatively more hydrophobic layer, which is bonded to the second nonwoven layer, swells less and results

30 in less puckering of the fabric when the outer surface of the garment is contacted with aqueous materials compared to a garment that is made with the second nonwoven layer facing towards the person wearing the garment.

Because the majority of the film layer is comprised of the comparatively more hydrophilic layer, the garment also maintains an excellent moisture vapor transmission rate to ensure the comfort of the wearer.

- Figure 3 illustrates a process for extrusion coating of a two-layer film onto a powder-bonded nonwoven layer. A first melt-processable polymer is fed in pellet form, along with any additives, into the inlet 26 of extruder hopper 24, while a second melt-processable polymer is fed in pellet form, along with any additives, into the inlet 26' of extruder hopper 24'. The polymer is melted and mixed in the screw extruders 20 and 20' at screw speeds that depend on the dimensions of the extruders and the properties of the polymer. The melted mixture is discharged from the extruder under pressure through heated lines to a melt combining block 34, where a multiple layer melt is formed that is extruded as a multiple layer film through flat film die 38. The polymer is discharged from the flat film die 38 at a temperature above the melting point of the polymer mixture, and preferably at a temperature in the range of 180 °C to 240 °C. The polymer melt 40 discharging from the flat film die 38 coats the powder-bonded nonwoven layer 12 provided from a supply roll 46. Preferably, the powder-bonded nonwoven layer 12 passes under the die 38 at a speed that is coordinated with the speed of the extruder so as to obtain a film thickness of less than 25 micrometers, preferably less than 19 micrometers, on the powder-bonded nonwoven layer. The coated web enters a nip formed between nip roll 52 and roll 54, which rolls are maintained at a temperature selected to obtain a composite laminated sheet with a desired bond strength and moisture vapor permeability. A water dip pan 56 with associated roll 58 can be used to increase the quench rate and to prevent sticking. Alternatively, a water mist applied to the film layer or a water bath associated with roll 52 may be used. An optional cooled quench roll 50 can be used to provide additional cooling prior to winding the composite laminated sheet product on collection roll 60.
- The second nonwoven layer 16 (Fig. 1) is preferably formed of fibers or filaments of a melt-processable polymer such as polypropylene, polyethylene, or polyester, that can be heat-sealed to form seams in medical

garments. Examples of nonwoven fabrics suitable as the second nonwoven layer include spunbond, hydroentangled, stitchbonded, and flash-spun plexifilamentary nonwoven fabrics. For example, Sontara® hydroentangled polyester fabrics or Tyvek® flash-spun polyethylene sheets, available from

- 5 DuPont, can be used as the second nonwoven layer in the composite laminated sheet of the invention. If a flash-spun sheet is used as the second nonwoven layer, it preferably has been point-bonded and softened to provide the desired hand and drapability. Spunbond polypropylene or polyester nonwoven fabrics are preferred. The second nonwoven layer preferably has
10 a basis weight in the range of about 0.5 oz/yd² to 2 oz/yd² (17 g/m² to 68 g/m²), more preferably in the range of about 0.8 oz/yd² to 1.2 oz/yd² (27 g/m² to 40.7 g/m²). Thicker layers generally result in stronger seam strength when medical garments are fabricated with heat-sealed seams with the second nonwoven layer forming the outer surface of the garment.

- 15 In a preferred embodiment, the second nonwoven layer is a polypropylene nonwoven fabric, such as a polypropylene spunbond fabric. Polypropylene melts at a lower temperature than polyesters such as poly(ethylene terephthalate), thus requiring lower temperatures for heat-sealing the seams of the medical garment. Heat-sealed seams are generally
20 formed by overlaying two of the composite laminated sheets with what will be the outer surface of the garment (e.g. spunbond polypropylene) facing each other. When a garment is formed with the second nonwoven layer forming the outer surface of the garment, a seam is formed by contacting the edge of the overlaid sheets with a heated bar which fuses both of the second
25 nonwoven layers to each other, thus forming a seam having a width approximately the same as the width of the heated bar. Lower heat-sealing temperatures are preferred since the film layer of the composite laminated sheet is less likely to melt or degrade during the heat-sealing process. It has also been found that when the second nonwoven layer is a polypropylene
30 nonwoven fabric, higher seam strength and higher hydrostatic head measured at the seam are obtained compared to polyester nonwovens.

The second nonwoven layer can be adhered to the extrusion-coated powder-bonded nonwoven web using conventional adhesive lamination methods including powder lamination, hot melt lamination, and wet adhesive lamination. The lamination is preferably done in a way that provides

5 a composite laminated sheet having the desired softness and drapability, and a moisture vapor transmission rate of at least 600 g/m²/24 hr, preferably at least 1000 g/m²/24 hr. In a preferred embodiment, the second nonwoven layer is joined to the film side of the extrusion-coated powder-bonded nonwoven web using an adhesive that has been applied in discrete areas

10 such that the two components are bonded intermittently to each other. For example, the adhesive can be applied in a pattern or as randomly oriented filaments. The adhesive is preferably applied at about 2 g/m² to 4 g/m². If the adhesive loading is too high, the composite laminated sheet will be stiffer than desired. If it is too low, the bond strength between the film and the second

15 nonwoven layer will be too low. Preferably the bond strength between the film and the second nonwoven layer is at least 50 grams/inch when the composite sheet material is either wet or dry, more preferably between 50 grams/inch and 300 grams/inch.

The extrusion coated powder-bonded nonwoven web is generally less drapable and more noisy than is desired for use in garments. This is believed to be due to the high degree of bonding between the film layer and the powder-bonded nonwoven layer due to the high degree of compatibility between these layers. Surprisingly, it has been found that when the second nonwoven layer is adhered intermittently to the side of the film layer opposite

20 that to which the powder-bonded nonwoven layer is adhered, the drapability of the composite laminated sheet of the current invention is significantly improved and the noisiness of the composite laminated sheet is significantly diminished, compared to that of the extrusion-coated powder-bonded web.

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When used for garment end uses such as medical gowns, the composite laminated sheet 10 preferably has a basis weight between about 1.2 and 3 oz/yd² (41 to 102 g/m²) and more preferably between about 1.8 and 2.5 oz/yd² (61 to 85 g/m²), a grab tensile strength of at least 11 lb/inch (1925

N/m), and more preferably at least 15 lb/inch (2625 N/m) in both the machine and cross directions, a hydrohead of at least 50 cm, and a moisture vapor permeability of at least 600 g/m²/24 hr, preferably at least 1000 g/m²/24hr.

The composite laminated sheet of the invention also provides a viral barrier, with no viral penetration detected in 24 hours when measured according to 5 ASTM F1671. The bond strength between the film and each of the nonwoven layers of the composite sheet is preferably at least 0.1 lb/in (0.18 N/cm), and more preferably greater than about 0.15 lb/in (0.26 N/cm).

When the composite laminated sheet is intended for use in 10 medical garments, the fibrous components of the powder-bonded nonwoven layer and the second nonwoven layer are preferably selected so as to have some degree of hydrophobicity. Fibers or filaments having hydrophilic finishes applied thereto are generally less preferred. Hydrophilic fibers or filaments can contribute to soaking of the nonwoven layers by fluids, such as 15 blood, by capillary action when the fluid contacts the edge of the fabric, such as may occur with the sleeve of a medical garment. Very fine fibers or filaments (low dtex per filament) have also been found to contribute to this problem. Preferably the fibrous components of nonwoven webs are no less than about 1 denier per filament (1.1 dtex), and more preferably no less than 20 1.5 denier per filament (1.65 dtex). Medical garments are preferably fabricated from the composite laminated sheet of the invention with the second nonwoven layer facing outwardly, away from the person wearing the garment. The second nonwoven layer is preferably treated with a repellent composition such as a fluorochemical treatment so that the second nonwoven 25 layer will more readily repel mixtures of alcohol and water.

As shown in the examples below, the use of a powder-bonded polyester nonwoven web as a supporting substrate for the extruded film layer instead of nonwoven fabrics that are conventionally used in disposable 30 medical garments, surprisingly allows thinner films and a lower overall basis weight to be used in the composite laminated sheet of the invention while providing superior viral barrier.

EXAMPLES

In the description above and in the non-limiting examples that follow, the following test methods were employed to determine various reported characteristics and properties. ASTM refers to the American Society for Testing and Materials, TAPPI refers to the Technical Association of Pulp and Paper Industry, ISO refers to the International Organization for Standardization and INDA refers to Association of the Nonwoven Fabrics Industry.

10 Basis weight was determined by ASTM D-3776, which is hereby incorporated by reference, and is reported in g/m².

15 Denier was determined by ANSI-ASTM D 1577-73, which measures weight in gram per 9000 meter in length of yarn.

20 Tensile strength was determined by ASTM D 5035-95, which is hereby incorporated by reference, with the following modifications. In the test a 2.54 cm by 20.32 cm (1 inch by 8 inch) sample was clamped at opposite ends of the sample. The clamps were attached 12.7 cm (5 in) from each other on the sample. The sample was pulled steadily at a speed of 5.08 cm/min (2 in/min) until the sample broke. The force at break was recorded in pounds/inch and converted to Newtons/cm as the breaking tensile strength.

25 Film thickness was determined by ASTM Method D177-64, which is hereby incorporated by reference, and is reported in micrometers.

30 Grab Tensile Strength was determined by ASTM D 5034-95, which is hereby incorporated by reference, was measured in pounds/inch and is reported in Newtons/cm.

35 Elongation to Break of a sheet is a measure of the amount a sheet stretches prior to failure (breaking) in a strip tensile test. A 1.0 inch (2.54 cm) wide sample is mounted in the clamps, set 5.0 inches (12.7 cm) apart, of a constant rate of extension tensile testing machine such as an Instron table model tester. A continuously increasing load is applied to the sample at a crosshead speed of 2.0 in/min (5.08 cm/min) until failure. The measurement is given in percentage of stretch prior to failure. The test generally follows ASTM D 5035-95.

Bond strength is measured according to a test that generally follows the method of ASTM D2724-87, which is hereby incorporated by reference. The test was performed used a constant rate of extension tensile testing machine such as an Instron table model tester. A 2.54 cm (1.0 in) by 5 20.32 cm (8.0 in) sample is delaminated approximately 3.18 cm (1.25 in) by initiating a separation between the fibrous web and the moisture vapor permeable film. The separated sample faces are mounted in the clamps of the tester which are set 5.08 cm (2.0 in) apart. The tester is started and run at a crosshead speed of 25.4 cm/min (10.0 in/min). The computer starts 10 picking up readings after the slack is removed, nominally a 5 gram pre-load. The sample is delaminated for about 12.7 cm (5 in) during which sufficient readings are taken to provide a representative average of the data. The average bond strength is given in g/inch. For samples that are peeled the entire 5 inches the average bond strength is considered to be the bond 15 strength. For wet testing, samples were immersed in water for 5 minutes, and excess water was removed by paper towels before testing.

Hydrostatic head was measured according to ISO 811, which measures the resistance to water penetration on a 7 in x 7 in (18 cm x 18 cm) test sample. Water pressure is applied to the fabric side of the test specimen 20 until the sample is penetrated by water at three places. The hydrostatic pressure is measured in inches and converted to SI units and is reported in cm of water. The equipment used to measure hydrostatic head is made by Aspull Engineering Ltd, England.

Moisture Vapor Transmission Rate (MVTR) is reported in g/m²/24 25 hrs and was measured with a Lyssy Instrument using test method TAPPI T-523.

Viral Barrier properties were measured according to ASTM F1671. ASTM F1671 is a standard test method for measuring the resistance of materials used in protective clothing to penetration by blood-borne pathogens. 30 According to this method, three samples of a sheet material being tested are challenged with 10⁸ Phi-X174 bacteriophage, similar in size to the Hepatitis C virus (0.028 micrometers) and with a surface tension adjusted to 0.042 N/m,

at a pressure differential of 2 psi (13.8 kPa) for a 24 hour period. Penetration of the sample by viable viruses is determined using an assay procedure. The test results are reported in units of Plaque Forming Units per milliliter PFU/ml. A sample fails if any viral penetration is detected through any of the samples.

- 5 A sample passes if zero PFU/ml were detected after the 24 hour test period.

A positive and negative control is run with each sample set. The positive control was a microporous membrane with a pore size of 0.04 micrometers which passed 600 PFU/ml. The negative control was a sheet of Mylar® film, which passed 0 PFU/ml.

- 10 Handle-o-meter was measured according to INDA Standard Test (IST) 90.3. IST 90.3 is a standard test method for measuring the resistance of a 4-inch by 4-inch test fabric to fold, which is an indicator for softness. The handle-o-meter was reported in gram force. For each direction, machine (MD) and cross (CD), test results from both surfaces were averaged.

- 15 Mullen burst was measured according to ASTM D-3786. ASTM D-3786 is a standard test method for measuring the resistance of a 4-inch by 5-inch test sample to bursting using a hydraulic diaphragm tester. The Mullen burst was reported in psi. For wet testing, samples were immersed in water for 10 seconds and excess water was removed by paper towels before 20 testing.

Fiber size was measured by capturing a test sample image by a camera and evaluating the picture by an image analysis program. The distance across fiber longitudinal edges was measured as a fiber diameter and the averaged fiber diameter was reported in micrometers.

- 25 Bending Length was measured according to ASTM D-5732. ASTM D-5732 is a standard test method of measuring the stiffness of a fabric. It is determined as the length that a test strip bends under its own weight. The length of the overhang was reported in cm.

- 30 Alcohol Repellency was measured by INDA IST 80.8. IST 80.8 is a standard test method for measuring the resistance of nonwoven fabrics to penetration by aqueous isopropanol solutions. The alcohol repellency was reported in ratings based upon alcohol concentrations. The highest number

of test solution that did not penetrate the test specimen within five minutes was recorded.

Electrostatic Decay was measured by INDA IST 40.2. IST 40.2 is a standard test method for measuring the time required to dissipate a charge from the surface of a test specimen. The test sample was charged by positive or negative high voltage (5000V) and time for the charge dissipation was measured. The electrostatic decay was reported in seconds.

Example 1

10 The powder-bonded nonwoven layer used in this example was a 100% polyester powder-bonded nonwoven web having a basis weight of 0.5 oz/yd² (17 g/m²) (obtained from HDK Company, Greenville, South Carolina).
15 The powder-bonded nonwoven layer was formed from DuPont Dacron® Type 54W polyester staple fibers 1.5 inches in length and having a denier per filament of 1.5 (1.7 dtex). A copolyester powder adhesive is used at a loading of 18 percent by weight based on the total weight of the powder adhesive and staple fibers in the nonwoven web.

20 The powder-bonded nonwoven web was extrusion coated with a polymer film layer of Hytrel® G4778 copolyether ester (melting point 208°C, vicat softening temperature of 175°C, a shore hardness of 47D, and a water absorption of 2.3%, sold by DuPont) using the process shown in Figure 2. The Hytrel® polymer was fed in pellet form into a screw extruder and melted at a temperature of 440°F (227°C) and fed to a 30 mil (762 µm) by 102 cm die opening in a heated die block maintained at 232 °C. The powder-bonded
25 nonwoven substrate was spaced about 12 inches (30.5 cm) below the opening of the die. The film was extruded at a rate of 116 ft/min (35.4 m/min) to obtain a film thickness of 0.55 mil (14 micrometers). The film was joined to the fibrous powder-bonded nonwoven substrate by passing the coated web through a pair of nip rolls with a nip roll pressure of 100 psi to form a
30 composite laminated sheet. The nip roll that faced the polymer melt was a silicone rubber roll having a matte finish. The quench bath temperature was maintained at a temperature of 80°F (27°C).

Comparative Examples A and B

Comparative Examples A and B, as indicated in Table 1 below, were formed in a manner similar to the composite laminates of Example 1, except that a spunbonded polypropylene was used as the nonwoven layer, in place of the 100% polyester powder-bonded nonwoven web. In the Comparative Examples A and B, the basis weight of the nonwoven spunbonded polypropylene fabric webs was varied between 0.5 and 0.75 oz/yd². The nonwoven webs of Comparative Examples A and B were bonded to the Hytrel® G4778 copolyether ester polymer film layer at a temperature of 470°F (243°C) in order to partially melt the polypropylene and provide adequate bonding to the Hytrel® film layer. It was necessary to add a compatibilizer (13wt% Bynel 50E631) to the Hytrel ® film layer to improve its bond strength to the polyolefin nonwoven webs of Comparative Examples A and B. This compatibilizer was not used in Example 1.

Comparative Example C

A 1 mil thick Hytrel® G4778 copolyether ester polymer film layer was extruded onto a 100% spunlaced polyester nonwoven web at a melt temperature of 450-460°F (232-238°C) at a nip pressure of 100 psi at 300 ft/min to produce a polyester film/polyester nonwoven composite for comparison to Example 1.

The comparisons between the characteristics of Example 1 and the comparative examples are set forth in Table 1, below.

TABLE 1

| Example # | Nonwoven Basis Weight (oz/yd ²) | Film Thickness (mil) | MVTR (g/m ² /day) | HH (inch) | Viral Barrier |
|-----------|---------------------------------------------|----------------------|------------------------------|-----------|---------------|
| Ex. 1 | 0.5 | 0.55 | 999 | >157 | Compliant |
| C.Ex. A | 0.5 | 1.15 | 1133 | 138 | Failed |
| C.Ex. B | 0.75 | 1.15 | 1254 | 113 | Failed |
| C. Ex. C | 1.2 | 1 | n/a | n/a | Failed |

The data in Table 1 indicate that the composite laminates utilizing powder-bonded nonwoven layers according to the present invention demonstrate unexpectedly good viral barrier properties relative to conventional composite laminates, even when the polymer film layer is less than one-half the thickness of
5 the conventional laminates. Likewise, the Example 1 laminate of the present invention has better liquid barrier property (hydrohead), while maintaining roughly equivalent MVTR to Comparative Examples A and B. Comparative Example C failed the viral barrier test, which indicates that even when the composite laminate has a 100% polyester nonwoven layer, unless the nonwoven layer is a powder-
10 bonded layer, it has insufficient viral barrier properties.

Example 2

The powder-bonded nonwoven layer (obtained from HDK Company, Greenville, South Carolina) used in this example was same as
15 Example 1 but the powder loading was increased to 20 percent by weight. The increase in the powder loading may improve surface abrasion resistance of the nonwoven and bonding strength of Hytrel film to the nonwoven.

The powder-bonded polyester nonwoven web was extrusion-coated with a polymer film of Hytrel® 8206 using the process shown in Figure
20 2 at Scapa Tapes, North America (located in Liverpool, NY). Hytrel® 8206, copolyether ester (melting point 200°C, vicat softening temperature of 151°C, a shore hardness of 45D, and a water absorption of 30%, sold by DuPont) was utilized. The film had a three layer structure from a coextrusion process by two extruders. All three layers consisted of Hytrel® 8206. In addition, 6 %
25 of a blue color concentrate compounded with Hytrel® 4056 was added into the extrusion hopper.

The Hytrel® polymer and additive pellets were dried and fed into the hopper and melted at 444 °F (229 °C). The barrel zone temperatures for the extruders were in the range of 455 (235) to 470 °F (243 °C). The heated
30 die block maintained its temperature in the range of 455 (235) to 496 °F (258 °C). The film was extruded to obtain a film thickness of 0.6 mil (15

micrometers). A nip roll pressure was 40 psi and the chill roll temperature was 55 °F (13 °C).

The physical properties of the bilaminate from Examples 1 and 2 are in Table 2.

5 Hytrel® 8206 was selected for Example 2 in order to reduce the noise level of the bilaminate, and also to increase the MVTR of the resulting bilaminate. Hytrel® 8206 has more ether than ester parts, resulting in a softer sheet material and a higher MVTR than sheet material made using Hytrel® G4778. Hytrel® G4778 has been found to provide greater strength and lower
10 water absorbency than Hytrel® 8206.

Table 2.

| | Polymer Film | Grab strength (lb) | | Elongation (%) | |
|-----------|---------------|--------------------|-----|----------------|-----|
| | | MD | CD | MD | CD |
| Example 1 | Hytrel® G4778 | 10.3 | 4.1 | 29 | 194 |
| Example 2 | Hytrel® 8206 | 14.5 | 5.4 | 18 | 99 |

| | Polymer Film | Handle-o-meter (g) | | Mullen Burst (psi) | | HH (inch) |
|-----------|---------------|-----------------------|-----|-----------------------|-----|--------------|
| | | MD | CD | Dry | Wet | |
| Example 1 | Hytrel® G4778 | 4.2 | 1.9 | 22 | 23 | >157 |
| Example 2 | Hytrel® 8206 | 7.2 | 1.9 | 24 | 20 | >157 |

| | Hytrel® | Bond strength - dry (g/in) | | Bond strength - wet (g/in) | | MVTR (g/m ² /day) |
|-----------|---------|-------------------------------|-----|----------------------------|----|---------------------------------|
| | | MD | CD | MD | CD | |
| Example 1 | 4778 | 144 | 120 | 27 | 52 | 999 |
| Example 2 | 8206 | 90 | 99 | 13 | 16 | 1282 |

5

Examples 3-26

In these examples, a second layer of a nonwoven fabric was added onto the two-layered composites from Examples 1 and 2 to form trilaminate structures. The bilaminates from the aforementioned extrusion coating process were laminated with a spunbonded polypropylene nonwoven

web having a basis weight of 0.6 oz/yd² obtained from BBA Nonwovens (located at Washougal, WA). For alcohol repellency and antistatic properties, the spunbonded polypropylene nonwoven was topically treated with a fluoroochemical and an antistatic agent. The physical properties of the 5 spunbonded nonwoven are in Table 3.

Table 3.

| Basis weight (oz/yd ²) | Thickness (mil) | Grab strength (lb) | | Elongation (%) | | Handle-o-meter (g) | | Fiber size (μm) |
|---------------------------------------|--------------------|-----------------------|----|-------------------|----|-----------------------|----|--------------------|
| | | MD | CD | MD | CD | MD | CD | |
| 0.6 | 9 | 7 | 6 | 27 | 41 | 4 | 2 | 23 |

| Bending length (cm) | Alcohol repellency (rating) | Electrostatic decay (sec.) | |
|---------------------|-----------------------------|----------------------------|------|
| | | + | - |
| 5.6 | 9 | 0.01 | 0.01 |

10 The above spunbonded polypropylene nonwoven was laminated with the composite sheet materials from Examples 1 and 2 by using a meltblown adhesive lamination technology. Three different types of hot melt adhesives were evaluated with add-on levels from 1 to 4 g/m². The adhesives, based on polystyrene-polyisoprene-polystyrene linear block 15 copolymers, H2465, H2485 and H2755, were provided by Bostik Findley (located in Wauwatosa, WI).

The hot melt adhesives were fed and melted in a hopper and transferred by an insulated hose into a 14-inch wide ITW Dynatec™ line at ITW Dynatec, An Illinois Tool Works Company (located in Hendersonville, TN) 20 equipped with nozzles having 7 holes/inch tips. The adhesive was melt-blown onto the Hytrel® side of the two-layered composites with a line speed of 600 ft/min, an air pressure of 18 psi and a nip pressure of 60 psi. The distance from the nozzle head to the bilaminate substrate was one inch. The

pump speeds for add-on levels of 1, 2, 3 and 4 g/m² were 15, 32, 47 and 59 rpm, respectively. The hopper, hose, head and air temperatures were selected based on the melt viscosity properties of the hot melt adhesives. For H2465, hopper, hose, head and air temperatures were 300, 325, 325 and 350 5 °F, respectively. For H2485, the processing temperatures were 350, 375, 400 and 420 °F. For H2755, the temperatures were 375, 400, 420 and 420 °F. The physical properties of the three layered composites are in Table 4.

Table 4.

| Example e No. | Adhesive e type | Bilaminate | Add-on (grams) | Bond strength - | | Bond strength - | |
|------------------|--------------------|------------|-------------------|-----------------|-----|-----------------|-----|
| | | | | dry (g/in) | MD | CD | MD |
| | | | | | | | CD |
| 3 | H2465 | Example 1 | 1 | 15 | 19 | 3 | 3 |
| 4 | H2465 | Example 1 | 2 | 77 | 38 | 9 | 7 |
| 5 | H2465 | Example 1 | 3 | 276 | 107 | 23 | 3 |
| 6 | H2465 | Example 1 | 4 | 129 | 144 | 17 | 12 |
| 7 | H2465 | Example 2 | 1 | 10 | 11 | 0 | 0 |
| 8 | H2465 | Example 2 | 2 | 44 | 48 | 0 | 0 |
| 9 | H2465 | Example 2 | 3 | 59 | 58 | 0 | 0 |
| 10 | H2465 | Example 2 | 4 | 107 | 122 | 0 | 0 |
| 11 | H2485 | Example 1 | 1 | 27 | 12 | 5 | 8 |
| 12 | H2485 | Example 1 | 2 | 41 | 71 | 15 | 26 |
| 13 | H2485 | Example 1 | 3 | 226 | 169 | 21 | 34 |
| 14 | H2485 | Example 1 | 4 | 157 | 148 | 29 | 33 |
| 15 | H2485 | Example 2 | 1 | 6 | 4 | 0 | 0 |
| 16 | H2485 | Example 2 | 2 | 31 | 16 | 0 | 0 |
| 17 | H2485 | Example 2 | 3 | 105 | 63 | 0 | 0 |
| 18 | H2485 | Example 2 | 4 | 118 | 50 | 0 | 0 |
| 19 | H2755 | Example 1 | 1 | 22 | 21 | 23 | 9 |
| 20 | H2755 | Example 1 | 2 | 91 | 11 | 84 | 65 |
| 21 | H2755 | Example 1 | 3 | 236 | 140 | 195 | 78 |
| 22 | H2755 | Example 1 | 4 | 287 | 142 | 253 | 237 |
| 23 | H2755 | Example 2 | 1 | 19 | 19 | 0 | 0 |
| 24 | H2755 | Example 2 | 2 | 113 | 105 | 0 | 0 |
| 25 | H2755 | Example 2 | 3 | 190 | 145 | 0 | 0 |
| 26 | H2755 | Example 2 | 4 | 117 | 215 | 0 | 0 |

The general trend from the bond strength tests indicates that the increase in the add-on levels of hot melt adhesive resulted in the increase in the bond strengths of the three-layered laminates. The results show that the trilaminates fabricated by using H2755 had higher bond strengths both in dry
5 and wet. The wet strengths from H2755 were significantly greater than those from other types of adhesives. The trilaminates including Example 2 had no wet strength due to the high water absorption (30%) of Hytrel® 8206. In the wet condition, the volume of Hytrel® 8026 film was increased and the trilaminates were easily delaminated. Therefore, high wet strengths were
10 obtained from the trilaminates having Example 1 as the bilaminate and H2755 as the hot melt adhesive.

The skilled artisan will recognize that the composite laminates according to the present invention can have use in a number of other possible applications in which moisture vapor permeability in combination with liquid
15 impermeability is important, such as protective covers for automobiles, crops, housewrap and roofliner. The viral barrier characteristics of the present invention also lend it to use in protective apparel other than medical garments, such as protective apparel to prevent particulate penetration, such as asbestos; protection from other biological agents such as bacteria; protection from harmful liquid
20 penetration, such as harsh chemicals; and cleanroom garments. Likewise, the composite laminates of the present invention can find use in personal care articles, such as diapers, sanitary napkins and the like. The vapor permeability of the present invention lends it to use in steam sterilization wraps for wrapping surgical instruments and supplies for sterilization.